

Investigating the Performance of Nano Composite Membrane Pebax/TiO₂ Nanoparticle Modified with Amino Silane in the Separation of CO₂ /CH₄

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ABSTRACT: In the current study, an in-depth examination was conducted to evaluate how the particle size of titanium dioxide (TiO₂) will affect the mechanical, thermal, and morphological properties of the modified Pebax/TiO₂ nanoparticle membrane. TiO₂ nanoparticles were initially modified with amino silane and then incorporated into the nanocomposite Pebax/TiO₂ membrane. The obtained membranes were characterized by FT-IR, SEM, TEM, TGA, and XRD to assess the effect of modification. The result of membrane performance evaluation indicated that the solubility of the gas molecules increased within the polymer matrix when an increase in CO₂ permeability was observed. To test the performance of the nanocomposite membrane in the high-pressure separation process, the feed pressure was increased from 2 to 10 bar and the results demonstrated that the CO₂/CH₄ selectivity boosted from 16.05 to 97.74, respectively. Furthermore, when the surface of TiO₂ nanoparticles was modified by amino silane and its concentration increased in the polymer matrix, the CO₂ permeability of the nanocomposite membrane increased from 87.12 to 24.71 compared to that of the pure Pebax membrane. Experimental data were correlated with ANN (artificial neural network. The ANN of the model applied in this study includes the Levenberg-Marquardt algorithm, purelin or a linear transfer function at the output layer, and tansig or a tangent sigmoid transfer function in the hidden layer with 5 neurons.

KEYWORDS: CO₂/CH₄ Selectivity; Permeability; Pebax/TiO₂ nanoparticle; Amino silane nanocomposite; Separation.

INTRODUCTION

Over the past decade, separation methods like chemical adsorption and cryogenic distillation as well as novel technologies like membrane process have gained popularity [1-4]. Moreover, industries are seeking novel methods to tackle environmental pollution, tackle energy consumption, and costs [5]. The matter of gas separation in many industrial applications is of significant importance [1, 6-10]. Besides, it requires lower

operating and maintenance costs, much more user-friendly, and has the least impact on the ecosystem as well [11-14]. In comparison to conventional available separation technologies, membrane-based gas separation offers numerous advantages including, occupying a relatively smaller footprint, cost-effective, process flexibility, and high energy efficiency [15, 16]. Even though inorganic

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membranes provide excellent gas separation performance along with high thermal and chemical stability, [17] they suffer from some challenges such as brittleness, high fabrication cost, nonscalability, and control over pore size. In contrary, polymeric membranes are attractive choices for separation applications owing to energy-effectiveness, low cost, and outstanding processability, and simplicity, and better scalability for large scale applications [18, 19].

In a study conducted by *Hassanajili et al.*, the productivity of the nanocomposite polyester membranes including metal nanoparticles was investigated for the separation of CH₄ and CO₂ pure gases. Based on their result, the gas permeability improved by increasing silica content, attributed to the increased free volume of the polymer network [20]. Such a similar trend was reported for several studies assessing the performance of polysulfone (PSF) Mixed Matrix Membranes (MMMs) with mesoporous silica MCM-41 for gas separation due to the excellent compatibility of the mesoporous materials with the polymer matrix which in turn improves the permeability of the PSF MMMs without sacrificing selectivity. Meanwhile, amine functionalized SBA-15 was reported to increase the CO₂/CH₄ selectivity in a study conducted by *Shimizu et al.* [21]. The addition of TiO₂ nanoparticles to poly (1-trimethylsilyl-1-propyne) (PTMSP) was investigated by *Matteucci et al.* and the findings revealed that the permeability CH₄, N₂ and CO₂ enhanced four times compared to that of the pure polymer [22]. In another research, they investigated the impact of TiO₂ nanoparticles on 1, 2-polybutadiene (PB) and the TiO₂ incorporated nanoparticles membrane demonstrated three times bigger permeability coefficients for CO₂, CH₄, N₂ and H₂ gases compared to that of the pure membrane, owing to the solubility coefficient of the gases [23]. Exploiting statistical modeling, the effect of diverse variables on the structural properties of the membranes was evaluated by incorporating Zinc oxide (ZnO), aluminum oxide (Al₂O₃), and titanium dioxide (TiO₂) nanoparticles to PMP membrane [24]. The embedment of inorganic nanomaterials into the polymers hold a special place in research due to their simplicity, mild operating conditions and stable performance [25]. Among various nanomaterials, TiO₂ nanoparticles is popular for its availability, photocatalytic activity, self-cleaning quality, ease of preparation and affordability [26]. However, the formation of TiO₂ agglomerates due to the high surface

energy at higher concentrations is a negative defect and its proper dispersion is a challenge [27]. Therefore, chemical or mechanical modification of TiO₂ nanoparticles will address this challenge. Silane coupling agents seems to be the most appropriate material for adjusting its surface properties [28], decreasing the agglomeration tendency and improving the compatibility with the polymer matrix [29]. This eventually lead to appropriate chemical or physical interactions with the polymer matrix [30].

Here, TiO₂ nanoparticles were initially modified with amino silane and then different content of modified TiO₂ nanoparticle (0.5 and 1 wt.%) were incorporated into the Pebax matrix, forming Pebax/TiO₂ nanocomposite membrane. The permeability, selectivity, and adsorption mechanism of the pure Pebax and Pebax/TiO₂ nanocomposite membranes were studied in detail for CO₂/CH₄ gas separation. After incorporation of the modified TiO₂ nanoparticles the CO₂/CH₄ selectivity and permeability of Pebax/TiO₂ nanocomposite membrane enhanced remarkably. Moreover, sorption studies, SEM, and tensile strength measurements were used to characterize the structure and properties of the pure and Pebax/TiO₂ nanocomposite membranes.

EXPERIMENTAL SECTION

Materials

All chemicals and solvents including Styrene, Propane diol, Toluene and n-Hexane were purchased from Merck and Aldrich Chemical Co. and were used without further purifications. TiO₂ nanoparticles with average particle size of 25–30 nm were purchased from Nanosabz Co. (Tehran, Iran) were dried at 500 °C for almost 5 h before utilizing to evaporated any possible humidity. T3-aminopropyltriethoxysilane (APTES) was also purchased used from Merck Chemical Co. and used as the coupling agent .

Identification and evaluation devices

The morphology of samples were analyzed with Transmitting Scanning Microscopy (TEM, JEOL) and scanning electron microscopy (SEM, KYKY-EM3200, Hitachi Company, China) under an acceleration voltage of 26 kV. Fourier transform infrared spectroscopy (FT-IR, Nicolet Co, USA) was used to study the functional groups on the surface of TiO₂ nanoparticles modified with amino silane. The tensile test of nanocomposite membranes

was conducted based on the ASTM-D3039 standards with the aid of Instron (6025K) at room temperature on specimens 150 mm long, 25 mm wide and 3 mm thick, with a machine speed of 5 mm / min. Correspondingly, the flexural strength of membrane samples was measured according to ASTM-D790 standard, using Instron (6025K) on specimens 90 mm long, 10 mm wide and 3 mm thick.

Synthesis of Pebax/TiO₂ nanocomposite membrane incorporated with amino silane modified TiO₂ nanoparticles

The casting solution of membrane was prepared by adding specific amount of Pebax (gr) to the THF solvent and the solution was stirred for 3 hours to form a homogeneous mixture. To attain such a solution, a two-step process was adopted; (i) 0.1 g of Pebax was dissolved in 2 mL THF and (ii) different quantities of m-TiO₂ NPs (m-TiO₂ nanoparticles, 0, 5, 10 and 15 wt%) were separately dispersed in 2 mL THF solution, under constant stirring for 24 h and at 25 °C. Then, two solutions were mixed to obtain the desired weight percentages of m-TiO₂ from 0.5 to 1.5 wt.%, Subsequently, the obtained mixture of nanocomposite Pebax/TiO₂ membrane nanoparticle solutions were stirred for 24h at 25°C. Afterwards, the mixture was subjected to ultrasonic ice bath for 2 h, with frequency of 2.259×10⁴ Hz and power of 100 W. The solution was transferred into the glass petri dishes for solvent evaporation at ambient temperature. The final nanocomposite Pebax/TiO₂ membranes modified with amino silane were collected after 1 day when solvent is completely evaporized [31].

Measurement and calculation method

The permeability of CO₂/CH₄ in the nanocomposite Pebax/TiO₂ membranes nanoparticle modified with amino silane were calculated by a constant pressure method (a soap bubble discharge gauge). The trial entailed a gas seepage cell in which one side was exposed to the membrane and the other side was in contact with the gas feed. By making use of a regulator, the pressure on the feed side was initially adjusted and then measured by a barometer. The following equation was used to determine the gas permeability of the membranes [32]:

$$\frac{P_i}{l} = \frac{1}{\Delta P} \frac{dv_i}{dt} \quad (1)$$

Whereby, P_i is the permeability of gas i , v_i is the volume of gas discharged into soap bubble discharge or

volume of gas permeability into the membrane in cubic centimeters, A is effective membrane surface area in square centimeter, t refers to bubble motion in column in seconds and ΔP shows the pressure drop across the membrane in centimeters of mercury. In case of GPU calculation, reports on the asymmetric membranes developed from the permeability division of the membrane thickness are available. Besides, the optimal selectivity of the two gases can be calculated via using the following equation:

$$\alpha_{i/j} = \frac{\left(\frac{P_i}{l}\right)}{\left(\frac{P_j}{l}\right)} \quad (2)$$

Where $\alpha_{i/j}$ is the optimal selectivity of gas i over j , P_i/l is the gas i permeability, and P_j/l is the gas j permeability.

Basically, it is generally accepted that the gas transfer properties of the organic/inorganic matrix membranes are hugely dependent on the membrane structure. The membrane structure is essentially dependent on the surface area and affinity between the particles and the polymer. Binomial absorption theory expresses the gas permeability in glassy polymers [33]. This theory introduces the total concentration of permeants (C) in the glassy polymer as a function of pressure (p), as follow:

$$C = k_D p + C'_H b p / (1 + b p) \quad (2)$$

Where K_D stands for the dissolution coefficient of artistic law and C'_H shows the cavity saturation constant. Moreover, b is the cavity continuity constant and demonstrates the ratio of the rate of constancy of absorption and desorption in the cavities. Taking into consideration that high porosity provides a place for the interaction between gases and the polymer network, the higher the porosity the higher the permeability and hence solubility.

Investigation the performance of membranes in terms of permeability and selectivity

Pressure-volume-constant-variable method can be utilized to verify the permeability prosperities of carbon dioxide and methane gases through polymeric membranes. Taking into account the steady-state conditions, the polymeric membranes developed in this method were initially pressurized for a specific duration of time

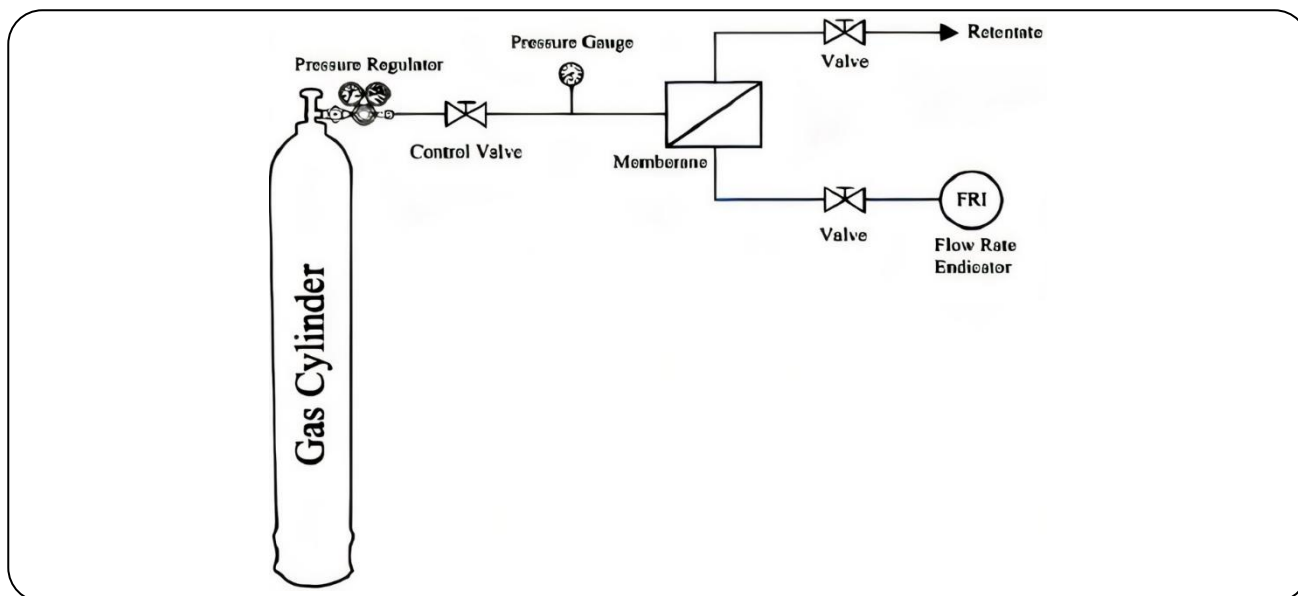


Fig. 1: Schematic permeability gas of the mixed matrix membranes.

and the volume flow rate through the membranes was recorded by a digital flow meter. The effective surface area of all membranes was estimated to be 56/71 cm². Every single permeability measurement was done at standard pressure and temperature. The polymeric membrane was fixed in the membrane tubes and then sealed by a hollow circular rubber ring. A gas feed inlet and two outlet portions were embedded in the membrane tube. From the two outlets, one was considered for the gas component leaked through the membrane and the other for the residual gas component. Fig. 1 represents the schematic of the apparatus applied to measure the leakage of carbon dioxide and methane from the polymeric membrane.

Artificial neural network

From the field of Artificial Neural Network model (ANN), back propagation algorithm as the training algorithm for a feed forward network has been applied. Initially, the model tried to compare the ultimate computed data for FFBP with the experimentally detected outcomes. After computation of the errors, they were used for adjusting each neuron weight. The evaluation of input variables including the CO₂/CH₄ selectivity and permeability, nanocomposite Pebax/TiO₂ membrane containing TiO₂ nanoparticle modified with amino silane, and pressure were performed all over the process. Subsequently, five neurons at 37 experimental points were employed to feed the model. Data adjustment was obtained by training, test, and

validation sets contained 50%, 25% and 25% data points, respectively. Due to the application of tan-sigmoidal transfer function all of the data points were normalized in the range of [0.1, 0.9] based on the ensuing Eq. (4) as follow [34]:

$$X_{\text{norm}} = \frac{X - X_{\text{min}}}{X_{\text{max}} - X_{\text{min}}} \quad (4)$$

By assuming X as a variable in the above formula, X_{min} and X_{max} are the minimum and the maximum values respectively.

RESULTS AND DISCUSSION

Characterization techniques

Examination of TiO₂ Surface Modification Process

Fig. 2 represents the FT-IR spectra of both unmodified and modified TiO₂ nanoparticles. Fig.2.a refers to the FT-IR spectrum of unmodified TiO₂ nanoparticles components while Fig. 2.b. represents that of the modified TiO₂ nanoparticles with amino-propyl triethoxy silane coupling agent. The peaks appeared around 1300 cm⁻¹ and 1320 cm⁻¹ can be contributed to the doublet from the asymmetric O=S=O stretching vibration and 1240 cm⁻¹ to the asymmetric C-O-C stretching vibration of the aryl ether group of the PES support layer, respectively [35-37]. The peaks observed at 1120 cm⁻¹ can be corresponded to the C-O-C symmetric vibration of ether group present in the PEO soft segment of the neat Pebax membrane [38, 39]. Two more peaks observed at about 1634 and 1744 cm⁻¹

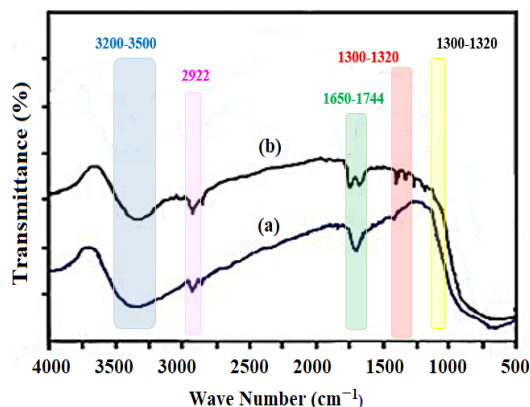


Fig. 2: (a) FT-IR spectra of the unmodified and (b) FT-IR spectra of the modified TiO₂ amino-propyl triethoxy silane.

can be referred to of the carbonyl groups the existing in the H-N-C=O and O-C=O segment of the PA part, respectively [40]. Moreover, the aliphatic -C-H band is identified at about 2922 cm⁻¹ [41]. The broad band appeared at 3398 cm⁻¹ can be correspond to the stretching vibration of -OH functions on TiO₂ NPs surface [42].

X-ray diffraction

The XRD patterns of UP, m-TiO₂ and UP with 0.5% and 1.0% of m-TiO₂ NPs are illustrated in Fig. 3. For pure UP (Fig. 3.d), it is apparent that there was a lack of diffraction signal in the range of 2θ angle barring one crystalline signal, suggesting the presence of a little proportion of crystalline phase. Since Pebax is a semi-crystalline polymer, XRD pattern of the neat membrane shows a weak diffraction peak due to the amorphous region and a strong diffraction peak owing to crystalline region of the polymer matrix. The peaks around 21° and 24° of 2θ can be contributed to the rigid segment while the small peaks at 2θ about 38-41° can be related to the crystalline phase of the soft segment in Pebax [45,46]. For m-TiO₂ NPs (Fig. 3a), the apparent signals at 101, 110, 004, 200, 105, 211, 204, 220, 301 prove the presence of rutile phase which is a good evidence of the crystalline form of this compound [27]. The change in the crystallinity of Pebax can prove the intermolecular interaction between TiO₂ NPs and Pebax matrix [47]. Additionally, the characteristic signals of m-TiO₂ and UP in the XRD patterns reveal that the preparation process and surface modification cannot change the morphology of NPs (Fig.3b and c). Following the Debye-Scherrer formula, the

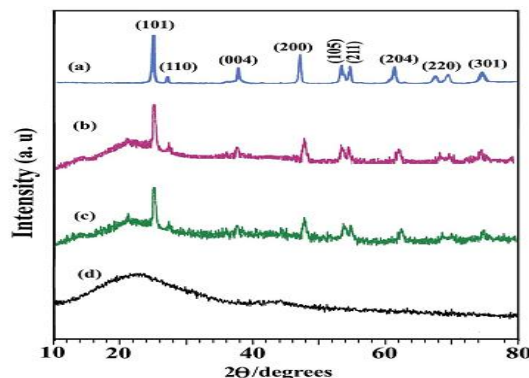


Fig. 3. XRD patterns of the surface modified TiO₂ (a), nanocomposite membranes with 0.5% (b) and 1.0% (c) of modified TiO₂ with amino silane and pure aromatic UP (d).

average size of the TiO₂ nanoparticles was estimated to be about 25–35 nm.

Morphology characterization of m-TiO₂ and UP/m-TiO₂ NCs

FE-SEM and TEM analysis were used to scrutinize the microstructures and nanofiller distribution within the NCs. The FE-SEM and TEM images of the m-TiO₂ with two distinct magnifications are displayed in Fig. 4 and 5. As clearly can be seen, the nanoscale size and globular shape of the m-TiO₂ NPs has been shown in the images. Furthermore, the sizes of particles were estimated to be in the range of 25–35 nm.

Thermal properties

ThermoGravimetric Analysis (TGA) TGA was conducted to assess the thermal decomposition temperature and weight loss of the of the modified-TiO₂, UP/m-TiO₂ NCs and pure UP under analysis. The thermal degradation behavior of the pure TiO₂ and Pebax/TiO₂ nanocomposite membrane is measured under nitrogen atmosphere and the results is illustrated in Fig. 6. As clearly be seen, silane surface modified TiO₂ NPs showed lower thermal stability compared to that of the pure one. The slight weight loss of unmodified TiO₂ NPs (roughly 2%) over the whole temperature ranges of 0–800°C could be ascribed to the elimination of water and partial dehydroxylation of the TiO₂ NPs. Based on TGA curve presented in Fig. 6b, the of m-TiO₂ demonstrated an evident two-step decomposition route, the former mass

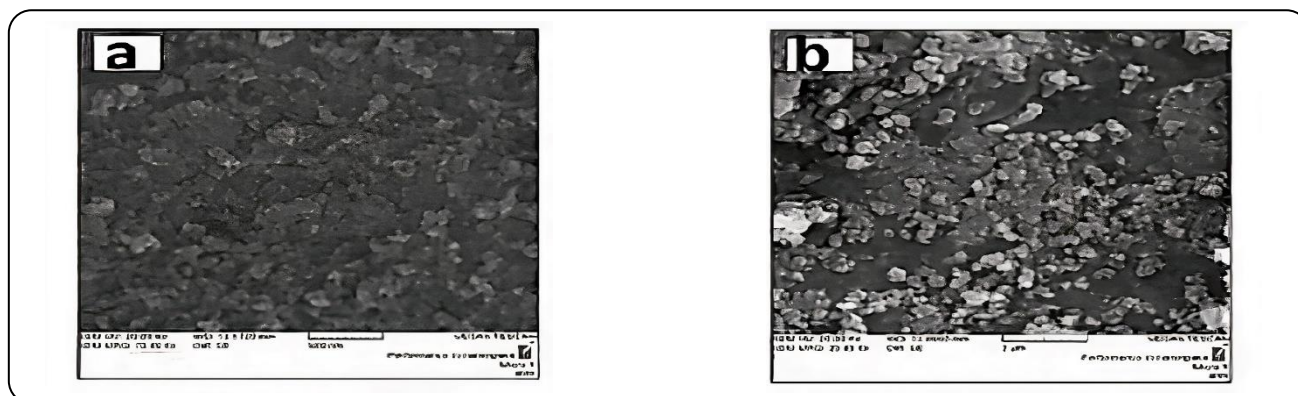


Fig. 4: (a, b) FE-SEM images of surface modified TiO_2 nanoparticles at different magnifications.

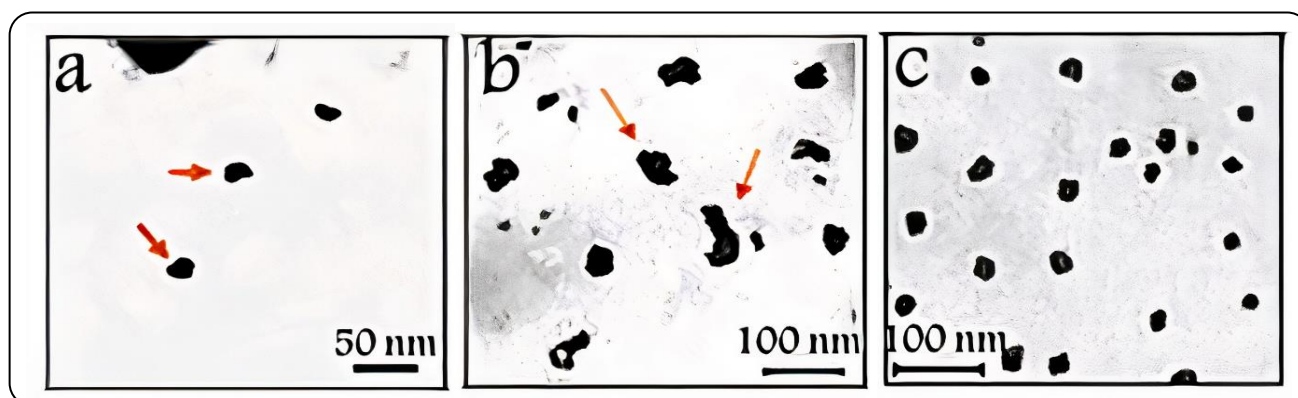


Fig. 5: (a, b, c) TEM images of surface modified TiO_2 nanoparticles at different magnifications.

loss occurs in the temperature ranges of 150–250 °C while the latter one observed at 450–550 °C. The first one could be attributed to the presence of hydroxide functional group on the surface of the TiO_2 NPs. Moreover, the TGA curves of the UP and UP/m- TiO_2 nanocomposite membranes are presented in Fig. 7 whereby a weight loss is observed by temperature increment. The gradual weight loss of the membranes can be ascribed to the decomposition of the polymer and the evaporation of entrapped solvent. To conduct a close examination of thermal stability, the TGA and weight loss of the UP/m- TiO_2 nanocomposite membranes containing 0.5 and 1.0 wt.% ($T_{0.5}$ and $T_{1.0}$) of m- TiO_2 NPs were measured over the temperature range of 0–800 °C (char yield). In parallel, as summarized in Table 1, the concentration of m- TiO_2 concentration in polymer matrix has a direct relation with the thermal stability. In other words, when higher concentration of m- TiO_2 is loaded into the polymer matrix, an increment of thermal stability will be observed owing to the formation of highly cross-linked network

structures. The primary reason behind such a finding can be attributed to the presence of m- TiO_2 nanoparticles which act as thermal insulator and also form a mass transport barrier to the volatile products produced during decomposition of the nanocomposite membrane. Besides, since the char yield is of prime importance for estimating the LOI Limiting Oxygen Index (LOI) values, the LOI was carried out for the UP/m- TiO_2 NCs over the range of 43–46%. Considering the definition, the Limiting Oxygen Index (LOI) is the minimum percentage of oxygen required for the combustion of materials and its value enhances with char yield increment, as stated by *Van Krevelen* [43]. Therefore, based on this explanation, nanocomposite membranes could be classified as the self-quenching materials.

$$\text{LOI} = 17.5 + 0.4\text{CR}, \text{ Where CR} = \text{char yield.}$$

Based on the estimation of LOI values carried out for UP/m- TiO_2 NCs in range of 43–46%, the NCs could be classified as the self-quenching materials.

Table 1: Thermal characterizations of the pure UP and nanocomposite Pebax/TiO₂ membrane containing different concentration of silane surface modified TiO₂ (UP/m-TiO₂ NCs).

Entry	Material	T ₅ (°C)	T ₁₀ (°C)	Char yield (%)	LOI (%)
1	Pure UP	397	437	59	41.7
2	UP/m-TiO ₂ NC0.5%	453	476	64	43.1
3	UP/m-TiO ₂ NC1.0%	496	512	69	45.1

^a Temperature at which 0.5 and 1.0 % weight loss was recorded by TGA at a heating rate of 20°C/min in a nitrogen atmosphere.

^b Percentage weight of material left undecomposed after TGA analysis at maximum temperature of 800°C in a nitrogen atmosphere.

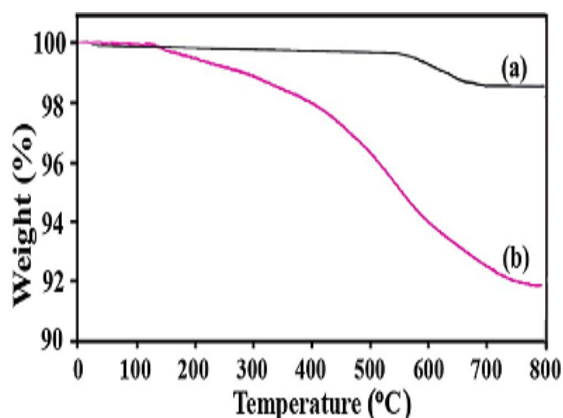


Fig. 6: TGA thermograms of pristine TiO₂ (a) and nanocomposite Pebax/ TiO₂ membrane containing modified TiO₂ (b).

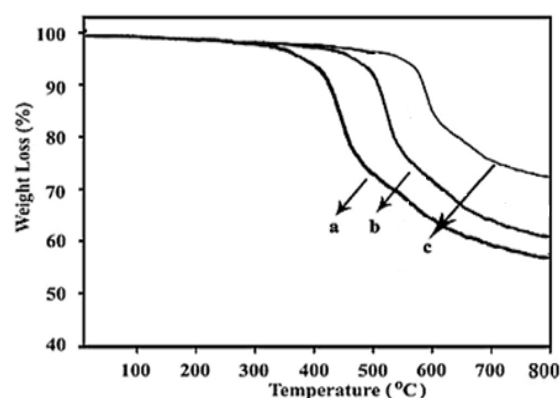


Fig. 7: TGA Thermograms of pristine UP (a), nanocomposite Pebax/TiO₂ membrane containing 0.5% (b), and 1.0% (c) silane surface modified TiO₂.

Physicomechanical properties of nanocomposite membranes

3.2.1. Morphology of prepared membranes

The SEM surface images of pure Pebax membrane showed filamentous fibers, while Pebax nanocomposite membrane containing amino silane modified TiO₂ nanoparticles presented multiple delaminated sheets on the surface. Considering the morphological properties, it can be said that a major transformation occurred from fibrous to pseudo-flowering from for the Pure Pebax and Pebax/m-TiO₂ nanocomposite membranes, respectively. Meanwhile, further evaluation on the surface changes of the pure and nanocomposite membranes proves that the apparent layers hardened the polymer-particle interface and an indistinct separation was also observed after modification [44].

Stretch test

The results of tensile strength nanocomposite membranes samples containing different concentrations of TiO₂ are presented in Fig 9-11; those of the elongation to

break of the samples in the tensile test are demonstrated. As displayed in Fig. 9, with each weight of the filler phase, the tensile strength of the pristine and nanocomposite membranes increases with the concentrations of TiO₂. In case of the nanocomposite membranes incorporated with m-TiO₂, higher tensile strength was observed compared to that of the unmodified TiO₂ NPs over the all concentration range tested in this study. Both nanocomposite membranes reinforced with unmodified and modified TiO₂ nanoparticles were analyzed. However, it should be pointed out that at the same weight percent, the nanocomposite reinforced with m-TiO₂ nanoparticles showed the greater tensile strength possibly because of higher interaction between nanoparticles and the polymer phase in the nanocomposite reinforced TiO₂ nanoparticles [45, 46]. Since TiO₂ nanoparticle were initially modified with amino silane and then incorporated to the Pebax matrix, the surface of the TiO₂ nanoparticle is covered with amine-functional groups. The amine terminals result in improved compatibility of TiO₂ inorganic nanoparticles

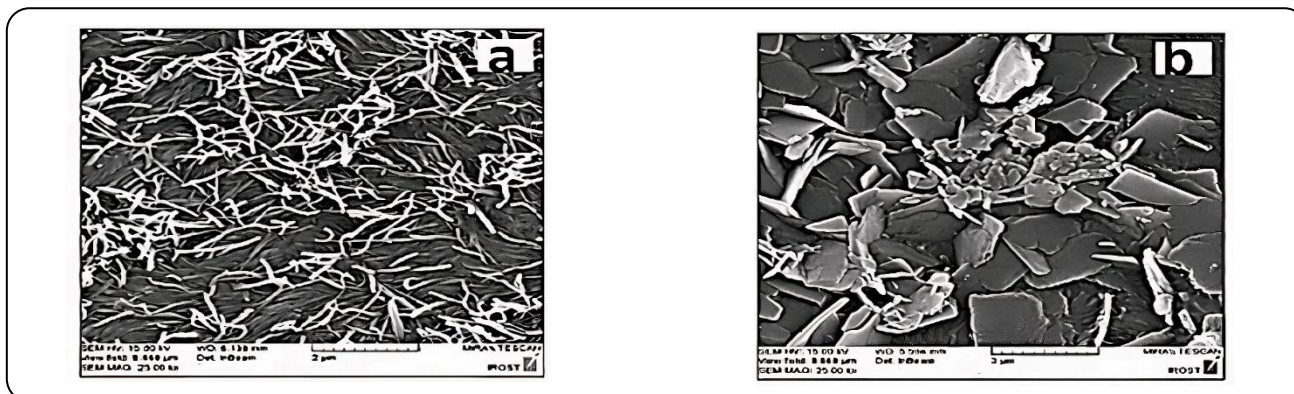


Fig. 8: SEM images of Membrane Surface (a) Pure Pebax Membrane and (b) nanocomposite Pebax/m-TiO₂ membrane Pebax Membrane.

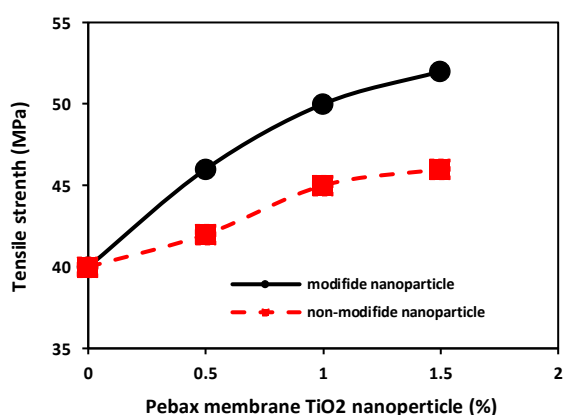


Fig. 9: Tensile strength of nanocomposite membranes containing different percentages and types of TiO₂ nanoparticles.

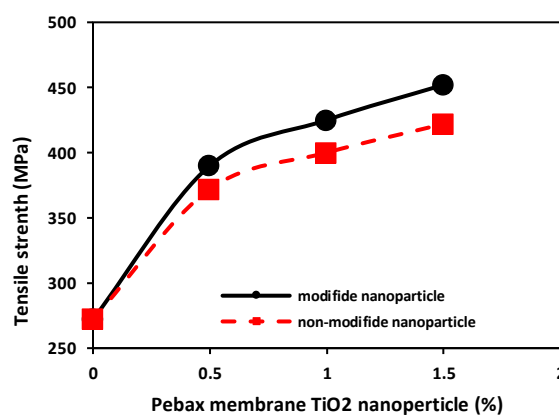


Fig. 10: Tensile models of nanocomposite membranes containing different percentages and types of TiO₂ nanoparticles.

with the Pebax polymeric chains and then increased dispersion occurs between two phases that in turn increases the elongation, tensile module, and flexibility of the final nanocomposite membranes [47]. Similar findings to were observed for the tensile modulus curve as represented in Fig. 10. However, as evident in Fig. 11, the elongation at break decreased with the concentration of TiO₂ NPs and the amount of this reduction was more evident in case of nanocomposite membranes reinforced with m-TiO₂ NPs.

Bending test

The results of bending test of all the membrane samples are shown in Fig. 12. In both cases of nanocomposite membranes incorporated with modified and unmodified TiO₂ NPs, the flexural strength improved with increasing the concentration of TiO₂ NPs. Greater flexural strength was spotted for the nanocomposite membranes reinforced

with m-TiO₂ NPs at the same weight percentages over all concentration ranges. This finding can be attributed to the presence of silane functional groups on the surface of m-TiO₂ ad it improves the affinity between metallic NPs and polymeric Pebax matrix. The higher the affinity of two phases, the more uniform the dispersion of NPs within the nanocomposite matrix and hence higher flexural strength was eventually observed.

Impact Test Results

Studying the dependence of on two factors:

It is generally accepted that the behavior of nanocomposite materials is dependent on two main factors namely NPs size, their interaction with the matrix phase and therefore distribution within the polymeric matrix. These factors are key prerequisite to achieve desired behavior [48]. The results of bending test of the membrane samples are displayed in Fig. 13. As evident, any rise

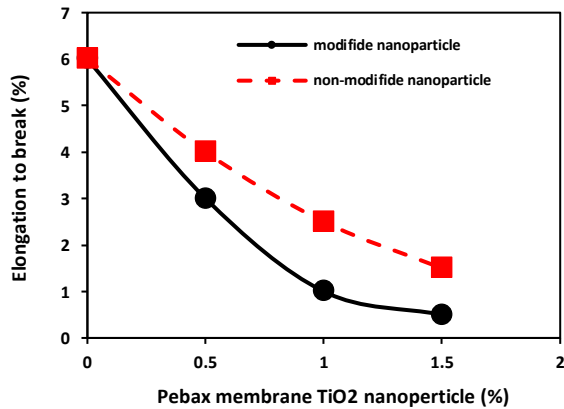


Fig. 11: The elongation to break of nanocomposite membranes containing different percentages and types of TiO₂ nanoparticles.

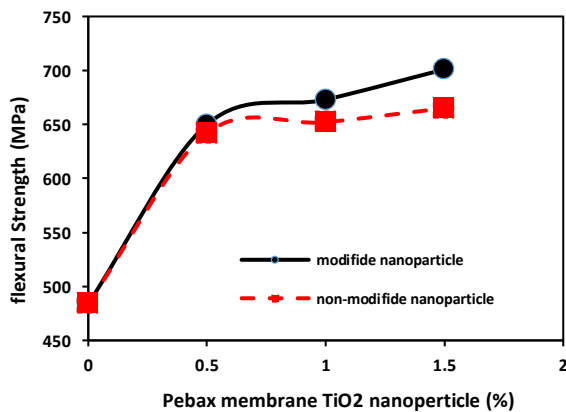


Fig. 12: The flexural strength of nanocomposite membranes containing different percentages and types of TiO₂ nanoparticles.

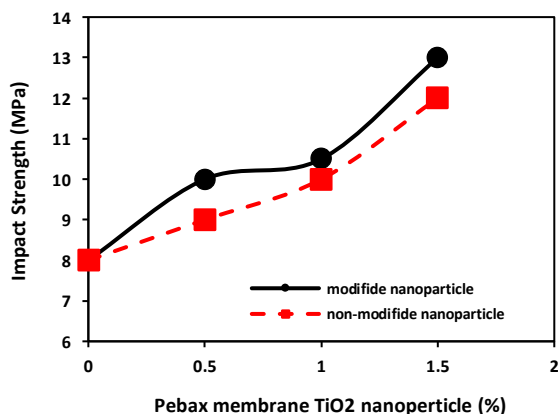


Fig. 13: The impact Strength of nanocomposite membranes containing different percentages and types of TiO₂ nanoparticles.

in the concentration of the TiO₂ NPs triggered enhanced the impact strength of both nanocomposite membranes incorporated with modified and unmodified TiO₂ NPs. However, this increase was remarkably apparent in case of m-TiO₂ NPs reinforced membranes. This behavior can be ascribed to the improved affinity and better distribution of NPs. It is believed that the presence of any agglomeration and bigger particle sizes can produce stress-focused areas and weaken the interaction between the nanoparticles and the polymer chains. Since unmodified titanium oxide NPs may result in occurring such challenges, the impact strength of the nanocomposite will finally reduce.

A thorough investigation was performed on the permeability and selectivity of carbon dioxide (CO₂) and methane (CH₄) for nanocomposite Pebax/TiO₂ membranes TiO₂ NPs modified with amino silane. The influence of these additives on the permeability of CO₂ and CH₄ in absence and presence of loading pressure are illustrated in Fig. 14 a, b. As crystal lucid, compared to that of the pristine Pebax membrane, the CO₂ permeability of nanocomposite membrane incorporated with m-TiO₂ NPs with amino silane increased with loading higher concentration of TiO₂ NPs. An enhancement from 24.71 to 87.12 was observed for the nanocomposite membrane containing 1 wt% of m-TiO₂ NPs. This increase can be corresponded to the presence of cavities due to the increase of free volume and the improved solubility of CO₂ inside the polymeric nanocomposite membranes. However, in both cases of the nanocomposite membranes containing modified and unmodified TiO₂ NPs, higher CO₂ permeability was observed compared to that of the CH₄ permeability [49]. Therefore, the recognition of the CO₂/CH₄ selectivity of is impossible (Table. 2) due to highly low value of the CO₂ permeability. However, the superior selectivity of the nanocomposite membranes as well as the unique properties of the membranes based on the Pebax copolymer can be confirmed by the results (Fig. 14 a, b).

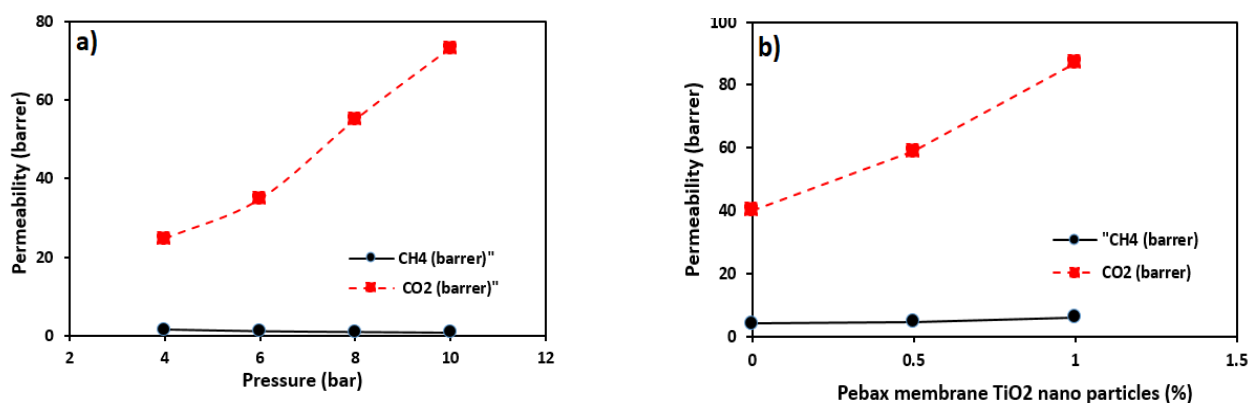
As summarized in Table 3, some major achievements are presented for the previously reported Pebax[®]1657 membranes including mixed matrix or blended ones in different fabrication conditions and operating conditions applied for CO₂/CH₄ separation. In comparison to the reported Pebax[®]1657 membranes, our modified TiO₂ nanocomposite membrane offer improved characteristic and gas separation performance, potentially great option to use in large scale gas separation plants.

Table 2: Separation performance for pure Pebax membranes (without TiO₂ NPs).

Pressure (bar)	Permeability (barrer)		Selectivity	membrane
	CO ₂	CH ₄		
4	24.71	1.54	16.05	pure Pebax membranes (without nanoparticles)
6	34.78	1.12	31.05	
8	54.97	0.928	59.23	
10	73.21	0.749	97.74	

Table 3: Summary of CO₂/CH₄ separation performance for several types of Pebax[®]1657 membranes modified with different types of additives.

Additive name	Loading (% wt.)	P (bar)	T (°C)	CO ₂ Permeance (GPU) (CO ₂ Permeability (Barrer))	CO ₂ /CH ₄ selectivity	Ref.
ZIF-8-IP	8	2	30	23.10 (261)	36	[50]
NaX-COOH	15	6	25	12.52 (187.8)	57.41	[51]
f-GO	0.7	2	35	(172)	17.1	[52]
Zn-TCPP	7	2	25	5.9 (626)	65	[53]
MCN	0.5	4	25	(123)	20	[54]
MIL-53(Al)	10	10	35	(129)	23.3	[55]
NH ₂ -MIL-53(Al)	10	10	35	(149)	20.5	[55]
UiO-66	2	7	25	14.8 (369.3)	31.3	[56]
UiO-66-NH ₂	1.5	7	25	15.7 (393.4)	39.8	[56]
MXene	0.1	4	25	1810	15	[18]
ZIF-8	20	3	25	(200)	15.1	[57]
ZIF-8	8	8	30	92.25 (655)	16.4	[58]
ImGO	0.8	8	25	(76.20)	30	[59]
CNF-UiO	3	6	25	13.14 (328.4)	27.4	[60]
NOTT-300	40	10	25	(395)	36.3	[61]
SiO ₂ -COOH	8	2	25	(133)	45	[62]
TEPA-MIL-101	5	4	25	19.43 (34.6)	46.33	[63]
CMC	3.75	4	25	14.85 (51.97)	47.22	[64]
Ni-NH ₂ -BDC	5	6	20	7.14 (31.55)	94	[47]
Pure Pebax	-	10	25	()	73.21	

**Fig. 14: The permeability of CO₂/CH₄ gases of the nanocomposite membranes containing TiO₂ NPs in a) absence and b) presence of applying pressure (4 bar).**

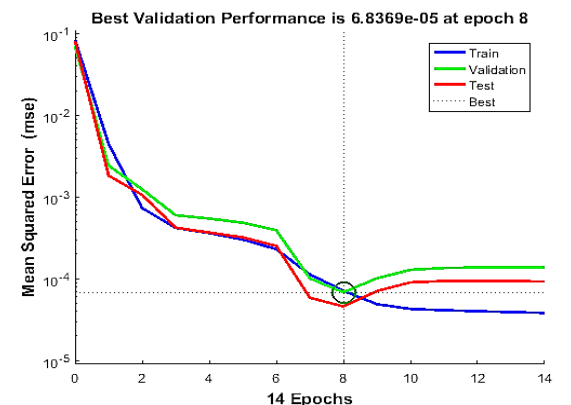


Fig. 15. Gradual change of training, validation, and test errors as a function of the number of training epochs during neural network model for CO₂ selectivity and permeability for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

Artificial Neural Network (ANN) modeling

Regarding the importance membrane-based gas separation technology, mathematical modeling provides a vital tool in the design process of the natural gas plants for CO₂ separation. The presence of reliable mathematical models for the performance prediction of the natural gas plants minimizes the technical risks [65-67]. Furthermore, it also eradicates the necessity of the time-consuming and expensive pilot plants and experimental studies to evaluate the operating conditions and membrane specification. Although the effectiveness of computational intelligence such as neural networks in engineering science has been demonstrated [68-72], few studies reported the use of ANN to evaluate the Pebax nanocomposite membrane performance. In this regard, we applied ANN analysis to validate the developed models based on the experimental data. Based on the obtained results, it was demonstrated that ANN modeling could be a good candidate for predicting the separation behavior of CO₂/CH₄ mixtures in Pebax/TiO₂ nanocomposite membrane in the absence of data from laboratory experiments. In this regard, three functions of weight (training), net input, and transfer (tansig) monitor and control the network function and performance. At epoch numbers 14, five neurons at 37 experimental points were selected. MSE (mean square error) of 0.607 in ANN model was spotted for CO₂/CH₄ selectivity and permeability. As it is evident from the plot of error histogram in Fig. 15-21, the errors are very negligible in this process. In this study, based upon the

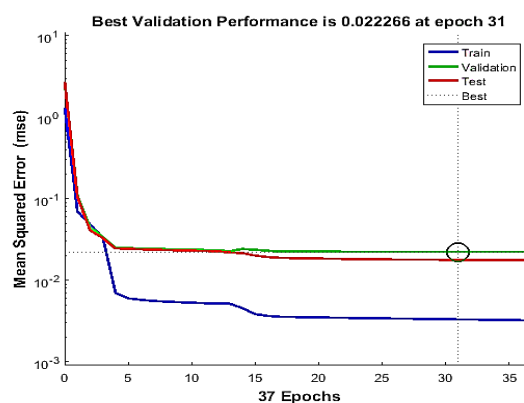


Fig. 16: Gradual change of training, validation, and test errors as a function of the number of training epochs during neural network model for CH₄ selectivity and permeability for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

function of error performance, the MSE had the minimum value at 5 neurons during the net training process [73, 74]. The ANN model with four input layers (including initial CO₂/CH₄ concentration, nanocomposite Pebax/TiO₂ membrane TiO₂ NPs modified with amino silane, pressure and Temperature) premised on the output layers (deletion of target compounds) was proved to be significantly reliable for predicting and reckoning the CO₂/CH₄ selectivity and permeability. Table. 4, 5 clearly present the MSE and the correlation coefficients (R²) for train, test, and validation of the CO₂/CH₄ selectivity and permeability.

The summary of the comparison of the error mean sum of squares, the mean absolute error, the standard deviation, the sum squares error, and the correlation coefficient for the findings of the model has been provided in Tables 4, 5. The results of ANN model demonstrated the relative superiority of the CO₂/CH₄ permeability of selectivity. Furthermore, the lowest permeability error clearly showed the perfect contribution of nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂ NPs modified with amino silane for the permeability of CO₂/CH₄ selectivity.

CONCLUSIONS

In the current study, the TiO₂ nanoparticle were initially modified with amino silane and then the permeability of TiO₂ nanoparticles incorporated Pebax nanocomposite membrane was tested by CO₂/CH₄ gas mixture at different pressures. The findings revealed that

Table 4: Juxtaposition of 1–22 neurons in the hidden layer for CO₂/CH₄ selectivity by ANN model development with the Levenberg–Marquardt algorithm.

Standard deviation	Average	High(+1)	Low (-1)	Parameter type	Factors
2.5	5.0	10	2	InPut Network	pressure (barrer)
1.0	0.75	1.5	0.5	InPut Network	membrane Pebax/TiO ₂ nanoparticle modified with amino silane nano composite (mol/L)
35	60	40	25	InPut Network	Tempreture
0.25	0.5	1.0	0.1	InPut Network	CO ₂ /CH ₄ selectivity
25.258	32.234	89.487	4.156	OutPut Network	% metronidazole drug

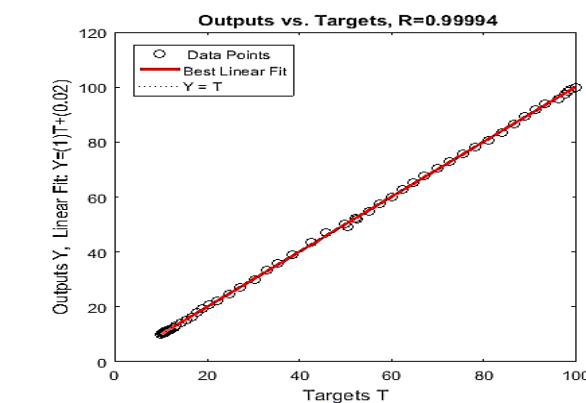


Fig. 17: Juxtaposition of Experimental (Objective) and Neural Network Outputs in Test and Total Data Stages for the CO₂ selectivity and permeability for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

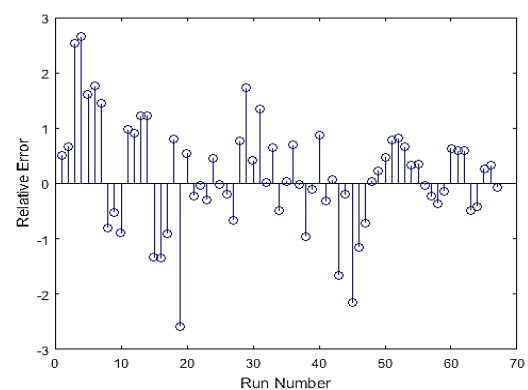


Fig. 19: The exhibition of the plot of Relative error histogram for permeability on the CO₂ selectivity for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

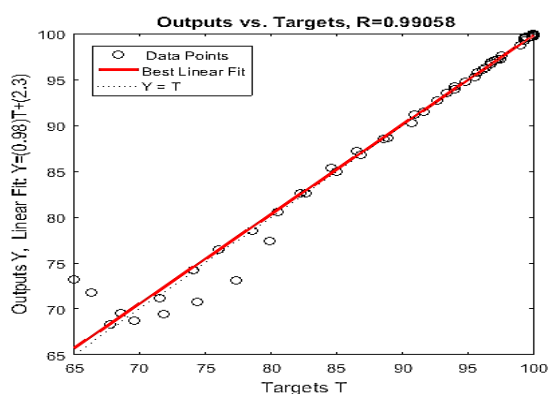


Fig. 18: Juxtaposition of experimental (objective) and neural network outputs in test and total data stages for the CH₄ selectivity and permeability for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

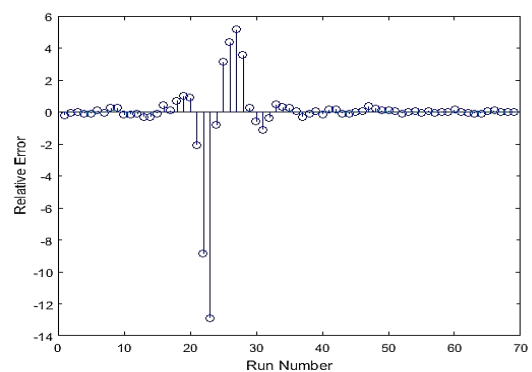


Fig. 20: The exhibition of the plot of relative error histogram for permeability on the CH₄ selectivity for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

Table 5: Statistical juxtaposition of three ANN models.

gas	SSE	MSE	AARE	SD	R ²
CO ₂	12.747	0.607	0.0362	0.4893	0.99983
CH ₄	10.815	0.515	0.0314	0.4539	0.99991

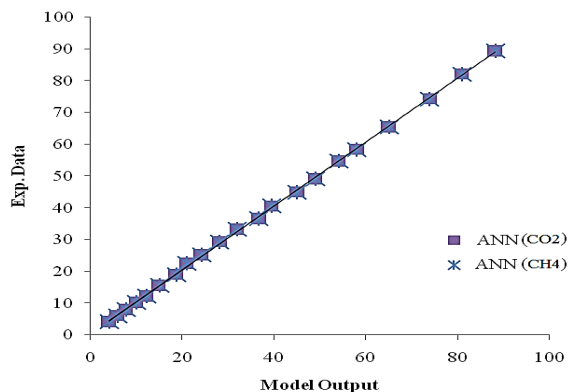


Fig. 21: The exhibition of the plot of juxtaposition of the outputs of all three models with experimental values for permeability on the CO₂/CH₄ selectivity for nanocomposite Pebax/TiO₂ membrane incorporated with TiO₂NPs modified with amino silane.

there is a direct relationship between the CO₂ permeability and the elasticity of the polymeric membrane, meaning the tensile strength can affect the CO₂ permeability at high pressures. In other words, elongation was observed for high concentrations of CO₂ absorbed onto the membrane surface, increasing the CO₂ permeability due to the improved solubility of the CO₂ molecules in the polymer matrix. Besides, there is inverse relation between CH₄ permeability and applied pressure whereby CH₄ permeability decreased by pressure increment. Additionally, the feed pressures increment resulted in improved performance and the selectivity of CO₂/CH₄ increased from 16.05 to 97.74 when the applied pressure enhanced from 2 to 10 bar. The same behavior was observed for the Pebax/TiO₂ nanocomposite membrane in which the CO₂ permeability nanocomposite membrane surged from 24.71 to 87.12 after amino silane modification. Meanwhile, such an ascending trend was also observed for CO₂/CH₄ selectivity of the nanocomposite membrane, as amino silane introduces numerous amin functional groups that have proper affinity to CO₂ polar molecules. To further assess the creditability of the results, the neural network analysis including three models was employed. Considering the permeability and CO₂/CH₄ selectivity

values after amino silane incorporation, the results confirmed that the Pebax/TiO₂ nanocomposite membrane provided the lowest errors. All these findings demonstrate superior performance of the nanocomposite membranes in terms of permeability and CO₂/CH₄ selectivity.

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