Numerical Investigation of Mixed Convection Flow of Viscoelastic Nanofluid with Convective Conditions over an Exponentially Stretching Surface

Bilal, Ashraf Mohammad*+

Department of Mathematics, COMSATS University Islamabad, Islamabad Campus, Islamabad, PAKISTAN

Mabood, Fazle

Department of Information Technology, Fanshawe College London, London, ON, CANADA

ABSTRACT: Numerical analysis is performed for a 3D incompressible viscoelastic nanofluid mixed convection flow model under the implications of convective boundary conditions towards an exponentially stretching sheet. The system that comprises differential equations of partial derivatives is remodeled into the system of differential equations via similarity transformations and then solved numerically through the Runge-Kutta-Fehlberg with shooting technique. The physical parameters, which emerge from the derived system are discussed in graphical formats. The significant outcomes of the current investigation are that the velocity field grows for a higher viscoelastic parameter while it reduces the fluid temperature. An increase in the mixed convection parameter diminishes the temperature and concentration. Further, the heat transfer rate is crumbled with the incremental values of the viscoelastic parameter. The obtained results show a better agreement with those available in the literature for limiting scenarios.

KEYWORDS: Viscoelastic fluid; 3D-flow; Mixed convection; Convective boundary conditions; Streamlines.

INTRODUCTION

Much deliberation in the inscription has been specified to the streams by a straight stretching surface. Nevertheless, this appears not practical when the procedures for plastic and polymer expulsion are thought of. In these dealings extending velocity is nonlinear. Extremely less consideration is given to the streams produced by power-law extending velocities. *Mgyari* and *Keller* [1] investigated the flow behavior and heat transfer due to the exponentially stretching of a surface with an exponential temperature distribution. *Okechi et al.* [2] presented the boundary layer analysis of flow-induced by rapidly stretching curved surfaces with exponential velocity. An investigative arrangement of the nanofluid stream over an exponentially extending surface was introduced by *Nadeem* and *Lee* [3]. Warmth move examination over an exponentially contracting surface through the shooting technique was researched by Bhattacharyya [4]. Numerical study of non-Newtonian fluid flow over an exponentially stretching surface: an optimal HAM validation was studied by *Rehman et al.* [5]. Double diffusive mixed convection flow from a vertical exponentially stretching surface in presence of the viscous dissipation was provided by *Patil et al.* [6]. The three-dimensional progression of thick liquid over an exponentially

^{*} To whom correspondence should be addressed.

⁺ E-mail: bilalashraf_qau@yahoo.com

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extending surface with heat move was concentrated by *Liu et al.* [7]. *Hayat et al.* [8] extended the work of *Liu et al.* [7] for viscoelastic fluid in the presence of thermal radiation and mixed convection effects.

Mabood et al. [9] deal with the magnetohydrodynamic flow and heat transfer over a permeable stretching sheet via the Homotopy Analysis Method (HAM). The effect of thermal radiation is included in the energy equation, while velocity and thermal slips are included in the boundary conditions. *Mabood et al.* [10] analyzed the hydromagnetic mixed convective flow with heat and mass transfer over a vertical plate embedded in a porous medium, they observed that the rate of heat transfer decreases with increased values of magnetic and slips parameters, *Motsa et al.* [11] tended to the progression of upper convected Maxwell liquid over a permeable extending sheet within the sight of a magnetic field.

Nanofluids have been proposed as a means for enhancing the performance of heat transfer liquids currently available, such as water, toluene, oil, and ethylene glycol mixture. Initially, the nanofluid term is used by Choi and Eastman [12]. Sheikholeslami et al. [13] presented a Control Volume-based Finite Element Method (CVFEM) on nanofluid radiative heat transfer analysis in a porous medium using Darcy Model, where they observed that the rise in Hatmann number reduce the Average Nusselt number while the radiation parameter uplifts it. Sheikholeslami et al. [14] introduced a new computational scheme for the exergy and entropy analysis of nanofluid in a porous medium, Hayat et al. [15] provided the study of Casson nanofluid over a stretching surface in presence of thermal radiation, heat source/sink, and first-order chemical reaction. Sheikholeslami and Ganji [16] examined the warmth move of Cu-water nanofluid streams between equal plates. Turkyilmazoglu [17] analyzed the flimsy blended convection stream of nanofluid over a moving vertical level plate with heat move. Ashraf et al. [18] tended to the three-dimensional progression of an Eyring-Powell nanofluid with convective limit conditions over an exponentially extending surface. After that mixed convection flow of magnetohydrodynamic (MHD) Jeffrey, nanofluid over a radially stretching surface with the radiative surface was discussed by Ashraf et al. [19]. Mabood et al. [20] investigated the heat generation/absorption and chemical reaction on a non-Newtonian (Sisko) nanofluid over a stretching surface under the influence of nonlinear radiation. *Mabood* and *Das* [21] presented the melting heat transfer of a nanofluid over a stretching surface taking into account a second-order slip model and thermal radiation. *Mabood et al.* [22] reported the combined effects of the chemical reaction and viscous dissipation on MHD radiative heat and mass transfer of nanofluid flow over a rotating stretching surface. *Sheikholeslami* and *Sadoughi* [23] detailed nanofluid convective stream within the sight of a liquefying surface. Nanofluid conduct in the presence of Coulomb force was shown by *Sheikholeslami* and *Chamkha* [2]. Some interesting features of nanofluids and heat transfer analysis can be found in Refs. [25-32].

Ashraf et al. [33] provided the mixed convection radiative flow of three-dimensional Maxwell fluid over an inclined stretching sheet in the presence of thermophoresis and convective condition. Soret and Dufour effects on the mixed convection flow of an Oldroyd-B fluid with convective boundary conditions was studied by Ashraf et al. [34]. Turkyilmazoglu [35] talked about the blended convection stream over a porous extending surface, where the author reported that the existence of unique or double solutions strongly relies on the Prandtl number, Mabood et al. [36] presented the heat transfer of micropolar fluid in the presence of binary chemical reaction and Arrhenius activation energy, it is mentioned that flow is undermined due to viscosity and buoyancy parameters which establishing the wider velocity boundary layer. Ashraf et al. [37] provided the mixed convection flow of Casson fluid over a stretching sheet with convective boundary conditions and Hall effect. Convective heat and mass transfer in the presence of chemical reaction and heat source/sink were studied by Ashraf et. al [38]. Sheikholeslami et al. [39] provided the magnetohydrodynamic nanofluid flow and convective heat transfer in a porous cavity.

From the aforementioned literature, the mixed convection viscoelastic nanofluid 3D flow with convective boundary conditions is not studied yet, to fill this gap, we examine the mixed convection flow of viscoelastic nanofluid with convective boundary conditions for heat and mass transfer over the exponentially stretching surface. Similarity transformations are utilized to reduce the partial differential equations into the ordinary differential equations. The resulting boundary layer system is solved by using Runge-Kutta-Fehlberg [40].

A variety of all the physical boundaries engaged with



Fig. A: Physical Problem.

the flow problem is analyzed for the flow field, temperature, and concentration.

THEORETICAL SECTION

Mathematical modeling

We talk about the blended convection limit layer stream of viscoelastic nanofluid over an exponentially extending surface. The surface agrees with the plane at z=0 and the stream is limited in the area z>0, as shown in Fig A.

Convective limit conditions for both warmth and mass exchange on the outside of a sheet are picked. The overseeing limit layer conditions for three-dimensional streams can be placed into the forms [18]:

$$\frac{\partial \mathbf{u}}{\partial \mathbf{x}} + \frac{\partial \mathbf{v}}{\partial \mathbf{y}} + \frac{\partial \mathbf{w}}{\partial z} = 0$$
(1)

$$u\frac{\partial u}{\partial x} + v\frac{\partial u}{\partial y} + w\frac{\partial u}{\partial z} = v\frac{\partial^2 u}{\partial z^2} +$$
(2)

$$\frac{k_0}{\rho} \left(u \frac{\partial^3 u}{\partial x \partial z^2} + w \frac{\partial^3 u}{\partial z^3} - \left(\frac{\partial u}{\partial x} \frac{\partial^2 u}{\partial z^2} + \frac{\partial u}{\partial z} \frac{\partial^2 w}{\partial z^2} + 2 \frac{\partial u}{\partial z} \frac{\partial^2 u}{\partial z^2} + 2 \frac{\partial w}{\partial z} \frac{\partial^2 u}{\partial z^2} + 2 \frac{\partial w}{\partial z} \frac{\partial^2 u}{\partial z^2} + 2 \frac{\partial w}{\partial z} \frac{\partial^2 u}{\partial z^2} \right) \right) + g \beta_C (C - C_{\infty})$$

$$\mathbf{u} \frac{\partial \mathbf{v}}{\partial \mathbf{x}} + \mathbf{v} \frac{\partial \mathbf{v}}{\partial \mathbf{y}} + \mathbf{w} \frac{\partial \mathbf{v}}{\partial z} = \mathbf{v} \frac{\partial^2 \mathbf{v}}{\partial z^2} +$$

$$\frac{\mathbf{k}_{0}}{\mathbf{p}} \left[\mathbf{v} \frac{\partial^{3} \mathbf{v}}{\partial \mathbf{y} \partial \mathbf{z}^{2}} + \mathbf{w} \frac{\partial^{3} \mathbf{v}}{\partial \mathbf{z}^{3}} - \left[\frac{\partial \mathbf{v}}{\partial \mathbf{y}} \frac{\partial^{2} \mathbf{v}}{\partial \mathbf{z}^{2}} + \frac{\partial \mathbf{v}}{\partial \mathbf{z}} \frac{\partial^{2} \mathbf{w}}{\partial \mathbf{z}^{2}} \right] \right] \\ + 2 \frac{\partial \mathbf{v}}{\partial \mathbf{z}} \frac{\partial^{2} \mathbf{v}}{\partial \mathbf{y} \partial \mathbf{z}} + 2 \frac{\partial \mathbf{w}}{\partial \mathbf{z}} \frac{\partial^{2} \mathbf{v}}{\partial \mathbf{z}^{2}} \right]$$

(3)

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$$u \frac{\partial T}{\partial x} + v \frac{\partial T}{\partial y} + w \frac{\partial T}{\partial z} = \sigma \frac{\partial^2 T}{\partial z^2} +$$

$$\frac{\rho^* c_p^*}{\rho c_p} \left(D_B \frac{\partial C}{\partial z} \frac{\partial T}{\partial z} + \frac{D_T}{T_{\infty}} \left(\frac{\partial T}{\partial z} \right)^2 \right)$$

$$\frac{\partial C}{\partial z} = \frac{\partial C}{\partial z} - \frac{\partial C}{\partial z} = \frac{\partial^2 C}{\partial z} - \frac{D_T}{\partial z} \frac{\partial^2 T}{\partial z} + \frac{D_T}{T_{\infty}} \left(\frac{\partial T}{\partial z} \right)^2$$
(4)

$$u \frac{\partial C}{\partial x} + v \frac{\partial C}{\partial y} + w \frac{\partial C}{\partial z} = D_B \frac{\partial^2 C}{\partial z^2} + \frac{D_T}{T_{\infty}} \frac{\partial^2 T}{\partial z^2}$$
(5)

Where the above conditions and *u*, *v*, and *w* are the velocity parts in the *x*-, *y*- and *z*- directions respectively, k_0 material liquid parameter, β_T warm extension coefficient, concentration development coefficient, D_B mass diffusivity, ρ^* density of nanoparticles, c_p^* specific heat of nanoparticles and prime denotes the differentiation with respect to η .

The boundary conditions can be expressed as follows:

$$u = U_{w}, v = V_{w}, w = 0, -k \frac{\partial T}{\partial z} = h(T_{f} - T),$$
 (6)

$$-D\frac{\partial T}{\partial z} = h^{*}(C_{f} - C) \text{ at } z = 0,$$
(7)

$$u \to 0, v \to 0, T \to T_{\infty}, C \to C_{\infty} \text{ as } z \to \infty$$
 (7)

$$U_{w} = U_{0}e^{\frac{x+y}{L}}, V_{w} = V_{0}e^{\frac{x+y}{L}}, T_{w} = T_{\infty} + T_{0}e^{\frac{A(x+y)}{2L}},$$
(8)
$$C_{w} = C_{\infty} + C_{0}e^{\frac{B(x+y)}{2L}},$$

By using the transformations [7]:

$$\begin{aligned} u &= U_{0} e^{\frac{x+y}{L}} f'(\eta), \ v = U_{0} e^{\frac{x+y}{L}} g'(\eta), \end{aligned} \tag{9} \\ w &= -\left(\frac{v U_{0}}{2L}\right)^{1/2} e^{\frac{x+y}{2L}} (f + \eta f' + g + \eta g'), \\ T &= T_{\infty} + T_{0} e^{\frac{A(x+y)}{2L}} \theta(\eta), \ C &= C_{\infty} + C_{0} e^{\frac{B(x+y)}{2L}} \phi(\eta), \\ \eta &= \left(\frac{U_{0}}{2v L}\right)^{1/2} e^{\frac{x+y}{2L}} z \end{aligned}$$

Eq. (1) is identically fulfilled and Eqs. (2)-(9) give:

$$f''' + (f + g)f'' - 2(f' + g')f' +$$
(10)

$$K \begin{pmatrix} 6f''f' + (3g'' - 3f'' + \eta g''')f'' \\ + ((4g' + 2\eta g'')f''' - (f + g + \eta g')f'''') \end{pmatrix}^{+}$$

$$2\lambda (\theta + N_r \phi) = 0,$$

$$g''' + (f + g)g'' - 2(f' + g')g' +$$
(11)

$$K \begin{pmatrix} 6g'''g' + (3f'' - 3g'' + \eta f''')g'' \\ + (4f' + 2\eta f'')g''' - (f + g + \eta f')g'''' \end{pmatrix} = 0$$

$$\theta'' + \Pr(f + g)\theta' - \Pr A(f' + g')\theta +$$
(12)

 $\left(N_{b}\theta'\phi'+N_{t}\theta'^{2}\right)=0$

$$\phi'' + S c(f + g)\phi' - S c A (f' + g')\phi + \frac{N_{t}}{N_{b}}\theta'' = 0$$
(13)

$$f = 0, g = 0, f' = 1, g' = \alpha, \theta' = -\gamma_1(1 - \theta(0)),$$
 (14)

$$\varphi' = -\gamma_2 (1 - \varphi(0)), \text{ at } \eta = 0$$

$$f' \rightarrow 0, \ g' \rightarrow 0, \ \theta \rightarrow 0, \ \phi \rightarrow 0 \ as \ \eta \rightarrow \infty \tag{15}$$

Where *K* viscoelastic parameter, λ mixed convection parameter, Gr_x local Grashof number, N_r concentration buoyancy parameter, Pr Prandtl number, *Sc* Schmidt number, α ratio parameter, γ_1 heat transfer Biot number and γ_2 mass transfer Biot number. These can be defined in the forms:

$$K = \frac{k_0 U_w}{2 v L}, \lambda = \frac{G r_x}{R e_x^2}, \quad G r_x = \frac{g \beta_T (T_f - T_\infty) x^3}{v^2}, \quad (16)$$

$$N_r = \frac{\beta_C (C_w - C_\infty)}{\beta_T (T_f - T_\infty)}, \quad P r = \frac{v}{\sigma}, S c = \frac{v}{D}, \alpha = \frac{V_0}{U_0},$$

$$\gamma_1 = \frac{h}{k} \sqrt{\frac{v}{a}}, \quad \gamma_2 = \frac{h^*}{D} \sqrt{\frac{v}{a}}$$

The heat transfer at wall and mass transfer at wall numbers in dimensionless forms can be expressed as follows:

N u / R
$$e_x^{1/2} = -\frac{x}{2L} \theta'(0)$$
 (17)

S h / R
$$e_x^{1/2} = -\frac{x}{2L} \varphi'(0)$$
, (18)

where $Re_x = \frac{U_o L}{v}e^{\frac{x+y}{L}}$ is the local Reynold number.

Numerical solution

The diminished conditions (10)- (15) are exceptionally non-direct and coupled and unraveled numerically utilizing Runge–Kutta–Fehlberg (RKF) with shooting technique for various estimations of boundaries. The effect of the different boundaries on the speed, temperature, concentration, warmth, and mass exchange rates are concentrated graphically. The step size is taken $\Delta \eta = 0.01$ furthermore, precision is up to the fifth decimal spot as the measure of combination. We expected an appropriate limited an incentive for the far-field boundary condition in (15), i.e. $\eta \rightarrow \infty$, say η_{∞} .

$$f'(\eta_{max}) = g'(\eta_{max}) = \theta(\eta_{max}) = \phi(\eta_{max}) \to 0$$

Figs. 1(a-c) are drafted to evaluate the impressions of the viscoelastic parameter K, the mixed convection parameter λ and the concentration buoyancy parameter N_r on the velocity profile $f'(\eta)$. It is to be found from Fig. 1a that the velocity profile $f'(\eta)$ enhances with an increase in the viscoelastic parameter K. As viscoelastic parameter Kis the ratio of wall velocity and kinematic viscosity. That's why as the viscoelastic parameter K enhances this means that the velocity of the fluid is more dominant than the viscosity of the fluid due to which velocity profile increases. It is to be depicted from Figs. 1b and 1c that within an increase in the mixed convection parameter λ and the concentration buoyancy parameter N_r the velocity profile $f'(\eta)$ increases. Figs. 2a-2c are sketched to discuss the impacts of ratio parameter α , temperature exponent A and heat transfer Biot number γ_1 on the velocity profile $f'(\eta)$. It is to be noted that the velocity profile and the momentum boundary layer thickness decrease within an enhancement in ratio parameter and temperature exponent A while the velocity profile and the momentum boundary layer thickness increase within an enhancement in heat transfer biot number γ_l . Variations of the viscoelastic parameter K, ratio parameter α and the mixed convection parameter λ on the secondary velocity profile $g'(\eta)$ are drawn in Figs. 3a-3c. It is to be observed that with in an enhancement in viscoelastic parameter K and ratio parameter α both the secondary velocity profile $g'(\eta)$ and the momentum boundary layer thickness enhances. It is also seen that the impact of the mixed convection parameter λ on the secondary profile $g'(\eta)$ is decreasing.

The influence of the *K*, λ , and *N_r* on the temperature $\theta(\eta)$ are analyzed in Figs. 4a-4c. It is to be noted that both the thermal boundary layer thickness and temperature profile $\theta(\eta)$ decrease within an increase in *K*, λ and *N_r*. Thermal boundary layer thickness decreases with an



Fig. 1: Effect of K, Nr and λ on velocity.



Fig. 2: Effect of α , A and γ on velocity.



Fig. 3: Effect of K, α and λ on secondary velocity.

enhancement in ratio parameter α and temperature exponent *A* while enhancing within an increase in heat transfer biot number γ_1 as seen in Figs. 5a-5c. Figs. 6a-6c are elucidated to discuss the impact of Prandtl number Pr, Brownian motion

parameter N_b , and thermophoresis parameter N_t on the temperature profile $\theta(\eta)$. It is noted that an increase in the Brownian motion parameter leads to an enhancement in the temperature $\theta(\eta)$ as well as the thermal boundary layer thickness.



Fig. 4: Effect of K, Nr and λ on temperature.



Fig. 5: Effect of α , A and γ_1 on temperature.



Fig. 6: Effect of Pr, B_b and N_t on temperature

Enhancement of thermophoresis parameters N_t and Pr reduces the thermal boundary layer thickness and the temperature $\theta(\eta)$. As Prandtl number Pr is the ratio of momentum diffusivity to thermal diffusivity which leads

to a decrease in both the thermal boundary layer thickness and the temperature $\theta(\eta)$ for increasing values of *Pr*.

Figs. 7-9 elucidates the variations of the *K*, λ , *N_r*, α , *A*, γ_l , *Sc*, *N_b* and mass transfer Biot number γ_2 on the



Fig. 7: Effect of K, λ and N_r on concentration.



Fig. 8: Effect of α , A and γ_1 on concentration.



Fig. 9: Effect of Sc, Nb, and γ_2 on concentration.

concentration profile $\phi(\eta)$. From these Figures It is to be found that the concentration profile $\phi(\eta)$ and the associated boundary layer thickness decreases with an increase in *K*, λ , *N_r*, α , *A*, *Sc* and Brownian motion parameter *N_b* while an increasing function of heat transfer biot number γ_l and mass transfer Biot number γ_2 . Figs. 10a-10b are plotted to analyze the effect of viscoelastic parameter *K*, mixed convection parameter λ , the concentration buoyancy parameter N_r , ratio parameter α ,



Fig. 10: Effect of K, λ , Nr & Pr, α , γ_1 on Nusselt number.

temperature exponent *A*, and heat transfer Biot number γ_1 on the local Nusselt number $-\theta'(0)$. These figures show that the enhancement of the viscoelastic parameter *K*, mixed convection parameter λ , the concentration buoyancy parameter N_r , ratio parameter α and heat transfer Biot number γ_1 enhances the heat transfer at the wall $-\theta'(0)$. Figs. 11a-11b are drawn to see the impacts of physical quantities on the Sherwood number $-\theta'(0)$. It is to be noted that Sherwood number $-\phi'(0)$ is an increasing function of viscoelastic parameter *K*, mixed convection parameter λ , the concentration buoyancy parameter N_r , ratio parameter α , mass transfer Biot number γ_2 and Schmidt number *Sc*.

Tables 1 and 2 are computed to see the comparison of the numerical values of the physical quantities with the *Hayat et al.* [8] and *Liu et al.* [7]. Table 3 is computed to see the impacts of the viscoelastic parameter *K*, mixed convection parameter λ , the concentration buoyancy parameter N_r , ratio parameter α , temperature exponent *A*, Schmidt number *Sc* and Brownian motion parameter N_b



Fig. 11: Effect of K, Nb, Nt & Sc, α , γ on Sherwood number.

while an increasing function of heat transfer biot number γ_1 and mass transfer biot number γ_2 on the local Nusselt number $-\theta'(0)$ and the Sherwood number $-\phi'(0)$.

Fig. 12 represents the streamlines for different values of the viscoelastic parameter (K= 0, 0.5, 1). It is seen that the streamlines diverge more and more from the origin for rising K. Divergence upgrades for K=0 compared to that for K=0.5, 1. Figures 13 manifests the isotherms for different values of the viscoelastic parameter (K= 0, 0.5, 1). More isotherms converge at the origin as we hike K. At K=0, the convergence is low as compared with other values of *K*.

CONCLUSIONS

The main outcomes of the present study are as follows.

- Increment in *K*, λ and *Nr* leads to the escalation of flow field $f'(\eta)$ while that of α , *A* curtail it.

- Rise in *K* upsurges $g'(\eta)$ while that of λ peters out it.

- Thermal field $\alpha(\eta)$ and the related boundary layer thickness gets diminished with proper increment in *K* and α .

($\alpha = 0$			$\alpha = 0.5$			$\alpha = 1$		
		[7]	[8]	Present	[7]	[8]	Present	[7]	[8]	Present
	-f"(0)	1.28180856	1.28181	1.281816	1.56988846	1.56989	1.569889	1.81275105	1.81275	1.812754
	-g"(0)	0	0	0	0.78494423	0.78494	0.784949	1.81275105	1.81275	1.812754
ĺ	$f(\infty)+g(\infty)$	0.90564383	0.90564	0.902727	1.10918263	1.10918	1.108288	1.28077378	1.28077	1.280462

Table 1: Comparison of -f''(0), -g''(0) and $f(\infty)+g(\infty)$ when $K=\alpha = \lambda = A = \gamma_1 = 0$.



Fig. 12: Contour plots of streamlines for different values of K.



Fig. 13: Contour plots of isotherms for different values of K.

Table 2: Comparison of $-\theta'(0)$ when K = 0.2, $\alpha = \lambda = \gamma_1 = 0.5$, Pr = 1.2, A = 0.2.

Hayat et al. [8]	Present
0.329701	0.3297095754

- Augmented γ_1 yield escalated concentration field $\theta(\eta)$.

- Rise in K and Pr improves heat transfer rate from stretching surface.

- Streamlines/Isotherms diverge/converge more and more from/to an origin accordingly.

К	λ	Nr	α	А	γ1	γ2	Sc	-θ'(0)	-\$(0)
0.0	0.2	0.2	0.3	0.3	0.1	0.1	0.2	0.085975	0.053716
0.5								0.087456	0.058471
1.0								0.087994	0.061029
0.2	0.5							0.087083	0.057522
	1.0							0.087374	0.059067
	2.0							0.087754	0.060985
	0.3	0.4						0.087089	0.057652
		0.7						0.087275	0.058749
		1.0						0.087421	0.059578
		0.2	0.0					0.085339	0.053987
			0.5					0.087753	0.058289
			1.0					0.089333	0.061977
			0.3	0.2				0.086175	0.054783
				0.6				0.088659	0.061307
				1.0				0.090244	0.065999
				0.5	0.2			0.157620	0.077943
					0.5			0.299248	0.024101
					1.0			0.426495	0.003819
					0.2	0.3		0.157579	0.098819
						0.6		0.157503	0.135109
						1.0		0.157452	0.158478
						0.5	0.5	0.156736	0.225039
							0.8	0.156481	0.274162
							1.5	0.156362	0.330229

Table 3: Numerical values of Nusselt and Sherwood numbers for various values of parameters when Pr = 0.7, Nb =	= Nt = 0.2.
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